

# Extending the Operating Range of Electric Spring Using Back-To-Back Converter: Hardware Implementation and Control

Shuo Yan, *Student Member, IEEE*, Chi-Kwan Lee, *Senior Member, IEEE*, Tianbo Yang, *Student Member, IEEE*, Kwan-Tat Mok, *Student Member, IEEE*, Siew-Chong Tan, *Senior Member, IEEE*, Balarko Chaudhuri, *Senior Member, IEEE*, and S. Y. (Ron) Hui, *Fellow, IEEE*

**Abstract**—This paper presents the first hardware implementation and control of an electric spring based on a back-to-back converter configuration. Because of its ability to provide both active and reactive power compensation, this back-to-back electric spring (ES-B2B) can substantially extend the operating range of the original version of the electric spring (ES-1) and provide enhanced voltage support and suppression functions. The hardware system and control of the ES-B2B have been successfully developed and tested. The experimental results have confirmed the effectiveness of the ES-B2B in supporting and suppressing the mains voltage. Particularly, the voltage suppression ability of the ES-B2B is superior over that of ES-1. The use of ES-B2B in a simulation study of a weak power grid has also been conducted. The ES-B2B has been found to be highly effective in mitigating voltage fluctuation caused by intermittent renewable power generation.

**Index Terms**—Adaptive systems, back-to-back converters, electric springs (ESs), smart grids, smart loads.

## I. INTRODUCTION

THE increasing use of intermittent renewable energy has posted new challenge to the power grid [1], [2]. The intermittent generation profile of renewable energy makes it difficult to maintain the supply-to-demand balance in real time. Traditional demand-side management approaches involve load shaving, day-ahead and hour-ahead forecasts, ON/OFF control of noncritical loads, and pricing policies [3]–[9]. As a demand-response technology with response time in the order of milliseconds, electric springs (ESs) have recently been proposed for providing future power grid with a range of attractive fea-

Manuscript received January 30, 2016; revised May 18, 2016; accepted August 28, 2016. Date of publication September 5, 2016; date of current version February 27, 2017. This work was supported by the Hong Kong Research Council through the Theme-based Research Project under Grant T23-701/14-N. Recommended for publication by Associate Editor J. M. Guerrero.

S. Yan, C.-K. Lee, T. Yang, K.-T. Mok, and S.-C. Tan Tan are with the Department of Electrical & Electronic Engineering, The University of Hong Kong, Hong Kong (e-mail: yanshuo@connect.hku.hk; cklee@eee.hku.hk; yang2014@connect.hku.hk; barrymok@connect.hku.hk; sctan@eee.hku.hk).

B. Chaudhuri is with the Department of Electrical and Electronic Engineering, Imperial College London, London SW7 2AZ, U.K. (e-mail: b.chaudhuri@imperial.ac.uk).

S. Y. (Ron) Hui is with the Department of Electrical and Electronic Engineering, The University of Hong Kong, Hong Kong, and also with Imperial College London, London SW7 2AZ, U.K. (e-mail: r.hui@imperial.ac.uk).

Color versions of one or more of the figures in this paper are available online at <http://ieeexplore.ieee.org>.

Digital Object Identifier 10.1109/TPEL.2016.2606128

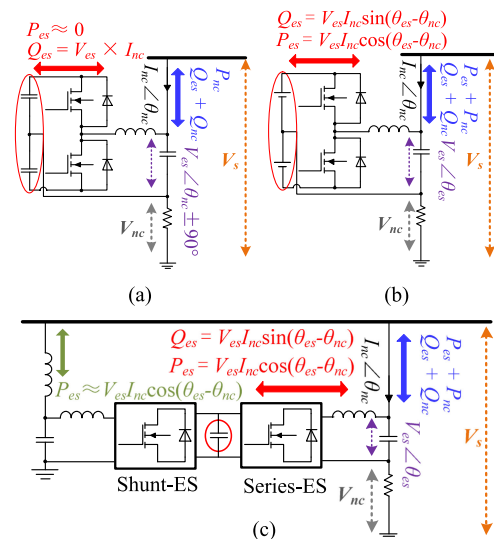


Fig. 1. Schematics of electric springs. (a) Electric spring version-1 (ES-1). (b) Electric spring version-2A (ES-2). (c) Electric spring version-2B (ES-B2B).

ture such as mitigation of voltage and frequency fluctuations [10]–[13], reduction of energy storage requirements [14], and reduction of power imbalance in buildings [15], [16]. So far, three versions of ES have been suggested. The original version (ES-1) involves a power inverter with a dc storage capacitor [10] as shown in Fig. 1(a). It is connected in series with a noncritical load. It provides direct reactive power compensation through the generation of a voltage in series with the noncritical load and indirect active power compensation through the modulation of the noncritical load power. The second version of ES (ES-2) is also connected in series with a noncritical load and consists of an active energy storage (such as a battery [17]) as illustrated in Fig. 1(b). Unlike ES-1, ES-2 provides both direct active and reactive power compensation and therefore has a much wider range. ES-1 has better voltage-support function than voltage-suppression function. This problem can be readily solved by using ES-2 at the expense of the requirement for a battery (that has maintenance and cost issues). While the ES-2 can be embedded in a noncritical load, a preferred option is to install it as part of the power supply infrastructure as shown in Fig. 2. In this new infrastructure for future power grid, the regulated

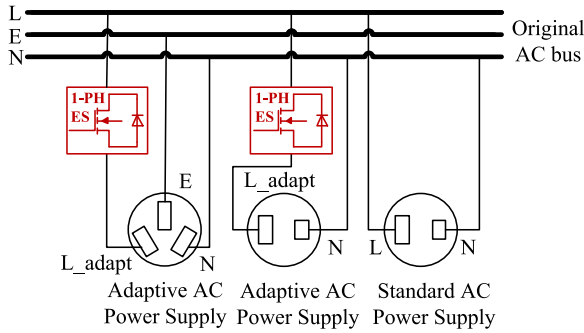


Fig. 2. Proposed new mains infrastructure for the future power grid.

mains can be considered as a standard mains, and the output of the ES can be treated as a new adaptive mains. Consumers using this adaptive mains with noncritical loads will be helping the utilities to stabilize the power grid with intermittent power sources. In this paper, the ES concept is explored with the practical use of a back-to-back converter configuration as shown in Fig. 1(c). It has the advantages of not using any battery because the dc voltage of the dc–ac power converter is provided by an ac–dc power converter. The operating principle of this back-to-back electric spring (ES-B2B) will be explained and practically verified with an experimental prototype.

## II. TOPOLOGY OF THE ES-B2B

This section explains the topology of ES-B2B and its benefits over other counterparts. Typical topologies of existing ESs include half-bridge inverter [10], full-bridge inverter [16], and three-phase inverter [15]. Either capacitor [10] or battery [17] has been used as energy storage. The first version of ES with capacitor (ES-1) has the advantage of simple implementation but shows a few operating limitations. As stated in [10], the output voltage of ES-1 is continuously modulated to be perpendicular with the noncritical load current. This control restriction limits the ES-1 in modulating the active power. Consequently, the ES-1 has good voltage supporting function and limited voltage suppression function. The ES proposed in [17] uses battery as energy storage (ES-2). Battery storage on the DC link allows the ES-2 to exchange active and reactive power with the grid. Therefore, the ES-2 voltage vector is no longer restricted to be perpendicular with the noncritical load current vector but can be set in any arbitrary angle. This version of ES has been used to conduct tasks such as voltage stabilization [13], power balance [15], [16], and power quality improvement [18].

The new ES-B2B consists of two half-bridge inverters configured in a back-to-back structure (see Fig. 3). One of the half-bridge inverter is used to be series compensator (Series-ES), and the other one to be a shunt compensator (Shunt-ES). The common dc link provides a channel for two-way power flow between Series-ES and Shunt-ES. The Series-ES possesses the operating modes of ES-2. The Shunt-ES is designated to cooperate with Series-ES by maintaining a stable voltage on the dc link. In addition, it can provide extra tasks such as reactive power compensation and harmonics cancellation.

An isolation transformer is connected on the output of the Series-ES to decouple the neutral point of Series-ES and

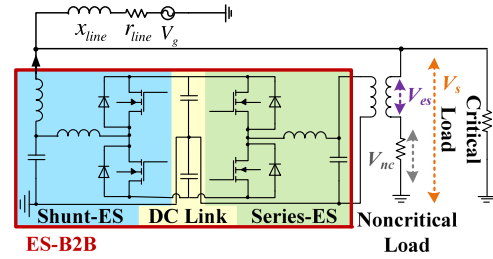


Fig. 3. Circuit diagram of the ES-B2B.

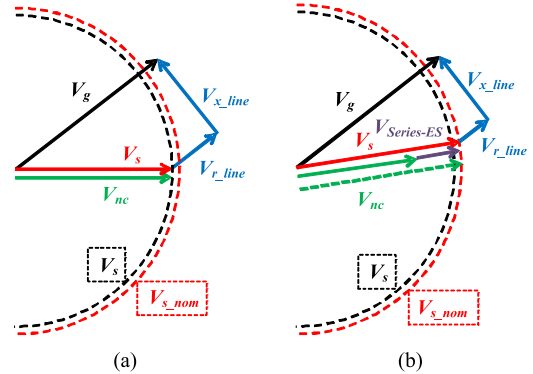


Fig. 4. Vector diagram of ES-B2B when supporting voltage. (a) Without ES. (b) With ES.

Shunt-ES. The secondary side of the isolation transformer is connected in series with the noncritical load to couple the compensation voltage into the system. This implementation inherits the function of the ES-2 that the bouncing effect of the compensation voltage can actively change the power consumption of the noncritical load. The output of the Shunt-ES is connected to the mains via an inductor.

The configuration of a bidirectional inverter as ES-B2B is different from a unified power flow controller. The Series-ES adopts an input control to regulate the mains voltage ( $V_s$ ) and provides an adaptive mains voltage ( $V_{nc}$ ) for the noncritical load (see Fig. 3). The series combination of the Series-ES and the noncritical load makes it possible to modulate the power of the noncritical load in order to balance supply and demand. Consequently, the noncritical load fed by the adaptive voltage output of the ES automatically becomes an adaptive load. Such adaptive (or smart) load can be regarded as a fast demand-response technology for the power grid. If those adaptive loads are distributed on the distribution network of the power grid, they form a robust stability support for the power grid.

## III. OPERATING PRINCIPLES OF THE ES-B2B

### A. Operating Modes of the ES-B2B

With Shunt-ES providing another channel of power flow, the ES-B2B possesses a highly effective ability to support and suppress the mains voltage. The vector diagrams of the simplified power grid with and without the support of the ES are shown in Figs. 4 and 5 for voltage support mode and voltage suppression mode, respectively. For the ease of analysis, the noncritical

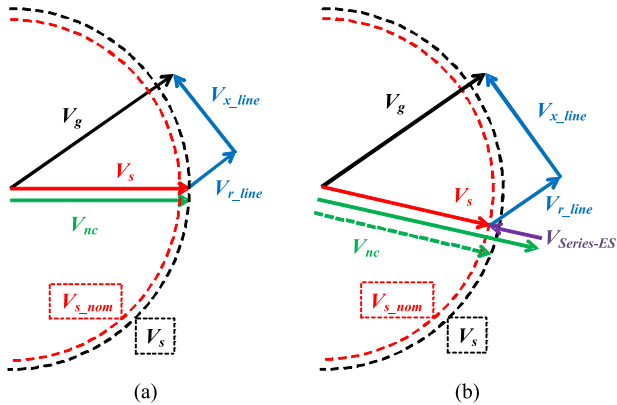


Fig. 5. Vector diagram of ES-B2B when suppressing voltage. (a) Without ES. (b) With ES.

load is assumed to be resistive, although it is not a necessary condition [17].

1) *Voltage Support Mode*: The ES will be operated under voltage support mode when the mains voltage falls below its nominal value. Before the ES-B2B is activated, both the noncritical load and the critical load are supplied with the mains voltage ( $V_s$ ) lower than its normal voltage ( $V_{s,nom}$ ), as shown in Fig. 4(a). When the ES-B2B is activated, a compensation voltage ( $V_{series-ES}$ ) in phase with the mains voltage ( $V_s$ ) can be introduced. This compensation voltage ( $V_{series-ES}$ ) suppresses the voltage of noncritical load ( $V_{nc}$ ) and thus reduces its power. The consequential reduction in line current results in the reduced voltage drop on the distribution line. The mains voltage can thus be supported up to its nominal value as shown in Fig. 4(b). The vector relationship between Series-ES voltage ( $V_{series-ES}$ ) and the noncritical load voltage ( $V_{nc}$ ) shows that the Series-ES operating in resistive mode absorbs active power from the grid and stores it in dc link. Due to the limited storage capacity, the Shunt-ES needs to deliver the absorbed power from the dc link back into the grid so that the capacitors would not be over charged and the dc voltage can remain constant. A power circulation is thus established in a way that the active power absorbed by Series-ES is continuously fed back into the grid by Shunt-ES and reused by Series-ES. This power circulation can effectively reduce the power consumption of Series-ES operating in resistive mode. As compared with the ES-2 with battery, the ES-B2B shows an enhanced ability to support voltage. When being activated to support the mains voltage, the ES-2 is operated in resistive mode and consumes active power. With no feedback channel, the absorbed energy has to be stored in the batteries. If this operation prolongs, a large battery capacity is required. In addition, the active power consumed by ES-2 could compromise the power reduction of the noncritical load intended for voltage support. Consequently, the voltage support function of the ES-2 is partially sacrificed by the resistive mode of the ES-2. With the power circulation made possible by Shunt-ES, this contradiction inherent in the ES-2 can be avoided by the ES-B2B topology.

2) *Voltage Suppression Mode*: When the mains voltage is higher than its nominal value, the vector diagrams without and with the ES-B2B are shown in Fig. 5(a) and (b), respectively.

TABLE I  
SPECIFICATIONS OF THE EXAMPLE FOR ES OPERATING RANGE

Symbol	Value
$V_s$ nominal value	220 V (RMS)
Nominal power	2 kVA, $PF = 0.85$
$V_{series-ES}$ (RMS)	0.68 p.u.
Power rating of Series-ES	0.50 p.u.
Voltage rating of Shunt-ES	1.00 p.u.
Power rating of Shunt-ES	0.50 p.u.
Noncritical load nominal power	0.55 p.u. (resistive)
Critical load nominal power	0.33 p.u., $PF = 0.80$

When the ES-B2B is activated, a compensation voltage ( $V_{series-ES}$ ) out of phase with the mains voltage ( $V_s$ ) is generated to boost the noncritical load voltage ( $V_{nc}$ ), as shown in Fig. 5(b). The original noncritical load voltage (highlighted in dotted green vector) is placed beside the compensated one. The introduction of ES voltage ( $V_{series-ES}$ ) causes power consumption of the noncritical load to increase, which increases the voltage drop on distribution line. The mains voltage ( $V_s$ ) is thus suppressed. The corresponding vector relationship between the Series-ES voltage ( $V_{series-ES}$ ) and noncritical load voltage ( $V_{nc}$ ) indicates that Series-ES is operated in negative-resistive mode when suppressing the mains voltage. When operating in negative-resistive mode, Series-ES supplies active power to the noncritical load. The Shunt-ES draws this active power from grid and delivers it to Series-ES via the dc link. The power transferred by the Shunt-ES increases the loading current and further reduces the mains voltage (due to the enlarged voltage drop on the distribution line).

### B. Operating Range and Limit of the ES-B2B

Similar to mechanical spring that cannot extend and retract infinitely, the ES-B2B must operate within its practical limits. The shunt structure and half-bridge circuit of Shunt-ES require that the dc voltage must be comparable to the voltage level of intended power grid. Once the dc voltage is stabilized, the Series-ES can generate compensation voltage to vary the power of the noncritical load. The stabilization of dc voltage requires that an active current must be exchanged between the Shunt-ES and the mains. The operating boundary of the ES-B2B can be determined with given ratings of the Shunt-ES and the Series-ES. The specifications of an example are tabulated in Table I. The oval area in Fig. 6 shows the compensation capacity of the ES-B2B, and the D-shaped area is that of the ES-1. It is clear that the ES-B2B can greatly expand the operating range of the ES.

## IV. CONTROL OF THE ES-B2B

The control of the ES-B2B needs to achieve a few targets:

- 1) the maintenance of a stable dc voltage;
- 2) the balanced power flow between Series-ES and Shunt-ES;
- 3) the extended voltage regulation function.

The scheme introduced in [19] uses the mathematic model of ES-B2B and assumes ES-B2B as a self-regulated entity, so

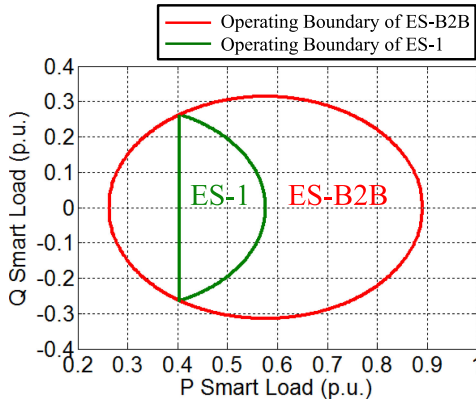


Fig. 6. Operating ranges of ES-B2B and the ES-1.

the inner power flow between Series-ES and Shunt-ES is not considered in the control loop. In hardware implementation, the cooperation of Series-ES and Shunt-ES is essential in the operation of the ES-B2B. Following those considerations, a detailed control scheme is discussed in this section.

For mains voltage regulation, the Series-ES can generate compensation voltage either in phase or out of phase with the mains voltage to adapt the power consumption of its associated non-critical load. Meanwhile, the Shunt-ES cooperates with Series-ES to stabilize the dc voltage and maintain a balanced power flow. Specifically, the negative-resistive mode (needed for the Series-ES to suppress the mains voltage) requires the Series-ES to release active power and Shunt-ES to acquire this active power from the grid. The resistive mode (needed for Series-ES to support the mains voltage) requires the Series-ES to absorb active power and the Shunt-ES to inject this active power back to grid.

To separate the control of active and reactive power of the ES-B2B, the controller is developed in a decoupled single-phase  $dq$  framework, where the mains voltage is chosen to be the reference vector with a phase angle of  $0^\circ$ . Equations (1) and (2) give the mathematic expressions of the single-phase polar to  $dq$  transformation. Mains voltage ( $V_s$ ), critical load voltage ( $V_{nc}$ ), and the current of Shunt-ES ( $I_{shunt-ES}$ ) are transformed into their respective  $d$  and  $q$  components in the control scheme

$$d = A \cos \theta = \frac{2}{T} \int_{T_n}^{T_n+1} A \sin(\omega t + \theta) \sin(\omega t) dt \quad (1)$$

$$q = A \sin \theta = \frac{2}{T} \int_{T_n}^{T_n+1} A \sin(\omega t + \theta) \cos(\omega t) dt. \quad (2)$$

In (1) and (2), the symbol  $A$  refers to the amplitude of currents or voltages,  $\omega$  is the fundamental angular frequency at which all decoupled  $d$  and  $q$  components are rotating, and  $\theta$  is the angle of currents or voltages with respect to the reference vector whose phase angle is tracked to zero degree by the phase-locked loop (PLL).

The implementation of single-phase  $dq$  transformation can facilitate the decoupling of active and reactive power control of the ES-B2B and thus simplify the control structure. Specifically, active power flow of the ES-B2B can be directly controlled by

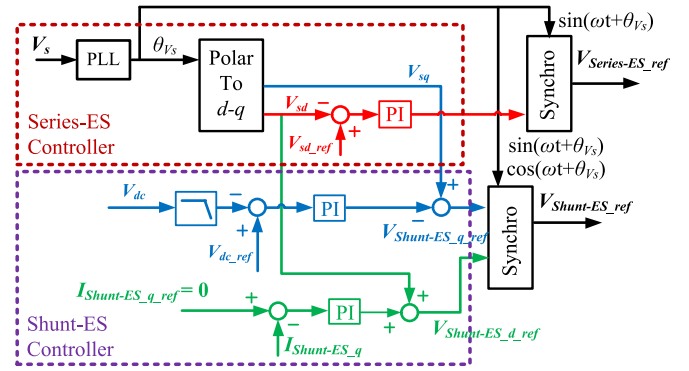


Fig. 7. Proposed control loop of ES-B2B.

modulating the  $d$  component of Series-ES voltage ( $V_{series-ES,d}$ ) and the  $q$  component of Shunt-ES voltage ( $V_{shunt-ES,q}$ ). The reactive power capacity of the ES-B2B can be applied to perform additional functions such as power factor correction and harmonic reduction, if necessary.

Fig. 7 shows the control diagram of the ES-B2B, in which three control loops are highlighted, respectively, in red, blue, and green colors. The control loop highlighted in red color is designated to operate the Series-ES for mains voltage support and suppression. This control loop follows the technique proposed in [20] that the Series-ES increases or decreases the supply voltage of the noncritical load while keeping its phase angle unchanged. Equation (3) is the mathematical expression of the voltage reference of the Series-ES. The  $d$  component of the mains voltage  $V_s$  ( $V_{sd}$ ) is fed back and compared with  $V_{s\_ref}$  (the nominal value of the mains voltage in a targeted power grid). The error signal is fed to a PI controller, which generates the  $d$  component of the Series-ES reference ( $V_{series-ES,d\_ref}$ ). A synchronization block is used to transform  $V_{series-ES,d\_ref}$  into sinusoidal form ( $V_{series-ES\_ref}$ ), which is kept in phase or out of phase with the mains voltage

$$V_{series-ES\_ref} = (V_{s\_ref} - V_{sd}) \left( K_{P1} + K_{I1} \frac{1}{s} \right) \cdot \sin(\omega t). \quad (3)$$

The use of the Series-ES to support and suppress the mains voltage requires the Shunt-ES to control the power flow in the ES-B2B via the regulation of dc voltage. The control loop highlighted in blue color (see Fig. 7) is designed for this purpose. The filtered dc voltage is compared with its reference. The error ( $V_{dc\_ref} - V_{dc}$ ) is fed to a PI controller to generate  $V_{shunt-ES,q\_ref}$  (the  $q$  component of Shunt-ES voltage reference), which controls the active current of Shunt-ES. In the proposed control scheme, the ES-B2B only uses its active capacity for voltage regulation. Its reactive capacity is deactivated by setting the reactive current reference of Shunt-ES equal to zero ( $I_{shunt-ES,q\_ref} = 0$ ). In the control block highlighted in green, the reactive current reference of Shunt-ES ( $I_{shunt-ES,q\_ref}$ ) is subtracted to  $I_{shunt-ES,q}$  (the reactive current of Shunt-ES). The error is fed to a PI controller to derive  $V_{shunt-ES,d\_ref}$  (the  $d$  component of Shunt-ES voltage reference). A

TABLE II  
 SPECIFICATIONS OF THE ES-B2B

Symbol	Value
Power switch	IRFP30N50
LCL filter	$L = 500 \mu\text{H}, C = 13.2 \mu\text{F}, L_g = 11 \text{ mH}$
LC filter	$L = 500 \mu\text{H}, C = 13.2 \mu\text{F}$
DC Capacitors	$C_1 = 6 \times 1500 \mu\text{F}, C_2 = 6 \times 1500 \mu\text{F}$
Switching frequency	30 kHz
Regulated DC-link voltage	360 V
Dead band	20 ns
Series-ES output voltage range (RMS)	0–80 V

synchronization stage is set to align  $V_{\text{shunt-ES}_d\text{-ref}}$  and  $V_{\text{shunt-ES}_q\text{-ref}}$ . The complete control loop of Shunt-ES is mathematically expressed as

$$\begin{aligned}
 V_{\text{shunt-ES-ref}} = & [V_{\text{sd}} + (I_{\text{shunt-ES}_q\text{-ref}} - I_{\text{shunt-ES}_q}) \\
 & \times \left( K_{P2} + K_{I2} \frac{1}{s} \right)] \cdot \sin(\omega t) \\
 & + \left[ V_{\text{sq}} - (V_{\text{dc-ref}} - V_{\text{dc}}) \left( K_{P3} + K_{I3} \frac{1}{s} \right) \right] \\
 & \cdot \cos(\omega t). \quad (4)
 \end{aligned}$$

## V. HARDWARE IMPLEMENTATION OF THE ES-B2B

The practical implementation of the ES-B2B consists of three segments:

- 1) the power electronic back-to-back converter circuit;
- 2) a sampling system and data-processing stage;
- 3) a controller designed for the mains voltage stabilization and dc voltage control of the ES-B2B.

The specifications of the hardware of ES-B2B implemented in a 110-V distribution grid are included in Table II.

Both half-bridge inverters in Fig. 3 use N-channel MOSFETs as power switches. Two sets of capacitors with 9000  $\mu\text{F}$  and 250 V voltage ratings are used to buffer energy for either positive or negative cycle. One half-bridge inverter of the ES-B2B is implemented as series-inverter (Series-ES). Its pulse width modulation (PWM) output voltage is filtered by an LC filter. The output of the Series-ES is a controllable sinusoidal voltage. The other half-bridge inverter is implemented as a shunt inverter (Shunt-ES), which is connected to the mains via an inductor.

The proposed controller is implemented in a dSpace 1104. Voltage and current sensors are used to capture the waveforms of Series-ES and Shunt-ES for control purpose and visualization. The sampling frequency of the controller is set at 10 kHz. The PWM generator has a switching frequency of 30 kHz and a dead band of 20 ns. Two digital input ports are used to provide the enable and disable signals for the Series-ES and the Shunt-ES.

## VI. EXPERIMENTAL AND SIMULATION RESULTS

In this section, the function of the ES-B2B to support and suppress the mains voltage is first demonstrated by experiments. The coordinated power flow of the Series-ES and Shunt-ES is practically evaluated. After verifying the functions of the

 TABLE III  
 SPECIFICATIONS OF POWER SYSTEM WITH ES-B2B

Symbol	Value
Power source	$V_{g,\text{nom}} = 110 \text{ V}$
Noncritical load	$40 // j116 \Omega$ (inductive plus resistive)
Critical load	$68 \Omega$ (resistive)
Line Impedance	$r_{\text{line}} = 0.7 \Omega, x_{\text{line}} = 4.9 \Omega$

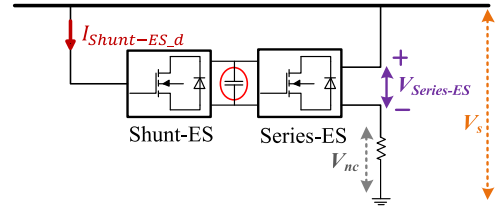


Fig. 8. Notations of measured variables of ES-B2B.

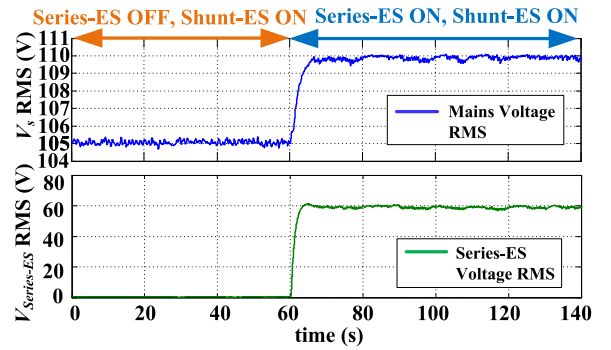


Fig. 9. Experimental mains voltage (upper trace) and the voltage of the Series-ES (lower trace) in voltage support mode.

ES-B2B experimentally, a circuit model is developed and used in a power simulation study. The hardware setup is based on the schematic in Fig. 3. A programmable power supply is used to emulate the power source. The nominal mains voltage is assumed to be 110 V. The programmable power supply is set at a voltage lower than 110 V in the voltage support tests and higher than 110 V for the voltage suppression tests. Table III gives the specifications of the hardware setup.

### A. Practical Tests on the Use of ES-B2B for Voltage Support

The first experiment is conducted to demonstrate the use of the ES-B2B to support the mains voltage. The notations of the measured variables are shown in Fig. 8. The power source is programmed to generate a voltage across the critical load at about 105 V (i.e., 5 V lower than the nominal value of 110 V). The ES-B2B is operated 1) with Shunt-ES maintaining a stable dc voltage and Series-ES bypassed and 2) with the Series-ES activated after the first 60 s. The measured mains voltage and the Series-ES voltage are shown in Fig. 9. It can be seen that at  $t = 60 \text{ s}$ , the Series-ES is activated and the mains voltage is restored to 110 V. The voltage support function of the ES-B2B is practically confirmed.

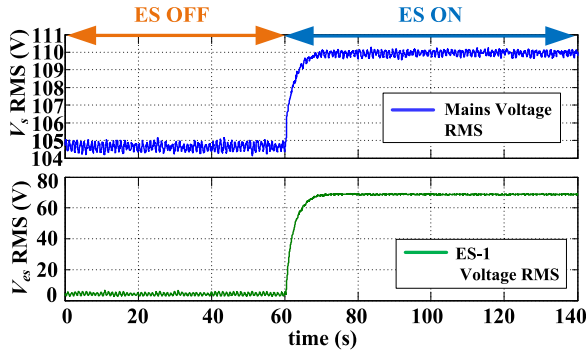


Fig. 10. Experimental mains voltage (upper trace) and the voltage of the ES-1 (lower trace) in voltage support mode. (For comparison with the results in Fig. 9.)

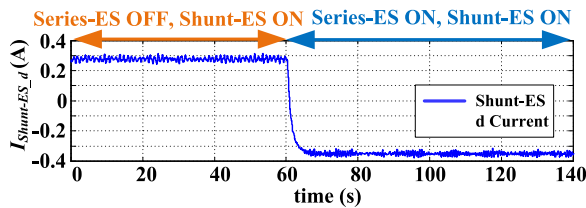


Fig. 11. Experimental active current of the Shunt-ES in voltage support mode.

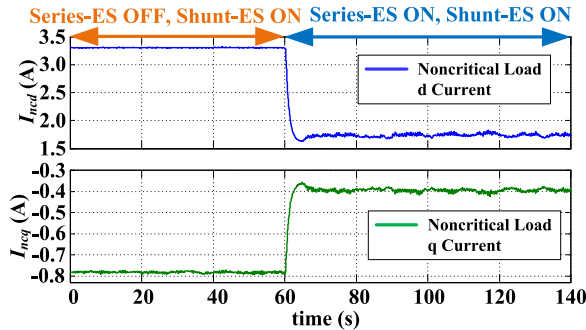


Fig. 12. Experimental active current ( $I_{ncd}$ ) and reactive ( $I_{ncq}$ ) current of the noncritical load in voltage support mode.

To highlight the effectiveness of ES-B2B in supporting the mains voltage, the measurement of the ES-1 working for the same function is shown in Fig. 10. After the ES-1 is activated at  $t = 60$  s, the mains voltage is restored to about 110 V, as expected. Therefore, both ES-B2B and ES-1 are capable of supporting the mains voltage. But the ES-B2B can react faster than the ES-1 and use less voltage capacity than ES-1 in accomplishing similar compensation results.

Other measurements of the ES-B2B under the voltage support mode are included in Figs. 11–13. In the first 60 s of Fig. 11, the Shunt-ES consumes a small amount of active current ( $I_{Shunt-ES,d}$ ) to compensate for the circuit loss in order to maintain a stable dc voltage. The current consumed by the noncritical load does not participate in compensation. At  $t = 60$  s, the Series-ES is activated to support the mains voltage. The compensation voltage ( $V_{series-ES}$  or the lower trace of Fig. 9) is in phase with the mains voltage and reduces the power of the

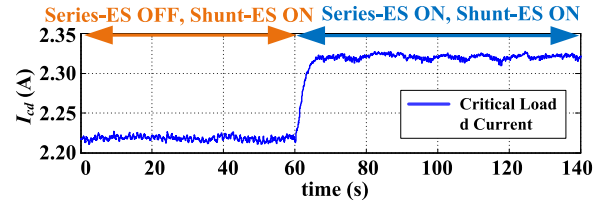


Fig. 13. Experimental active current of the critical load in voltage support mode.

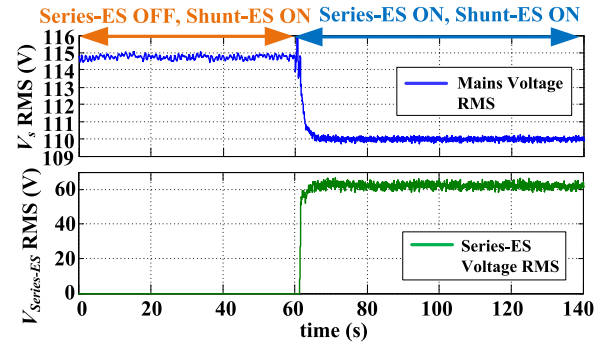


Fig. 14. Experimental mains voltage (upper trace) and the voltage of the Series-ES (lower trace) in voltage suppression mode.

noncritical load. As a result, the active and reactive current of the noncritical load ( $I_{ncd}$  and  $I_{ncq}$  in Fig. 12) is reduced after  $t = 60$  s. The Shunt-ES is adjusted to cooperate with the Series-ES. Since the Series-ES operates in resistive mode to support the mains voltage, the absorbed power is delivered to the dc link and circulated through the Shunt-ES back to the mains. This is evidenced by the reverse of the  $I_{Shunt-ES,d}$  from positive to negative in Fig. 11. In Fig. 9, the voltage bouncing effect of the Series-ES restores the mains voltage to 110 V after  $t = 60$  s. The supported voltage causes the active current of the critical load ( $I_{cd}$ ) to increase as shown in Fig. 13.

### B. Practical Tests on the Use of ES-B2B for Voltage Suppression

The second set of experiment was conducted to evaluate the voltage suppression function of the ES-B2B. The programmable power supply was set at 115 V (i.e., 5 V higher than the nominal value). The difference between the performance of the ES-B2B and the original ES-1 can be clearly observed as addressed in the following discussion.

The ES-B2B is initiated with its Shunt-ES in action for providing a regulated dc link voltage and its Series-ES kept in an idle state. The Series-ES is turned ON at  $t = 60$  s. The measured mains voltage and the voltage of the Series-ES are shown in Fig. 14. It can be seen that the ES-B2B can effectively suppress the mains voltage from 115 to 110 V. For the same test conditions with the use of ES-1, a set of waveforms are included in Fig. 15. Comparing the upper traces of Fig. 14, Fig. 15 indicates that ES-1 is not as effective as the ES-B2B in suppressing the mains voltage. The main reason is that the ES-1 does not have direct control of active power as the ES-B2B does. The ES-B2B does not have the limitation that the phasor relationship between

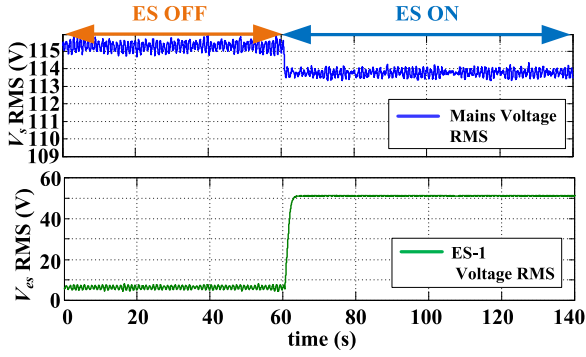


Fig. 15. Experimental mains voltage (upper trace) and the voltage of the ES-1 (lower trace) in voltage suppression mode. (For comparison with the results in Fig. 14.)

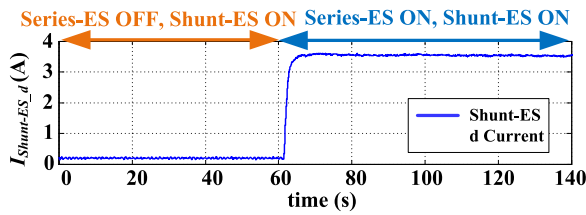


Fig. 16. Experimental active current of the Shunt-ES in voltage suppression mode.

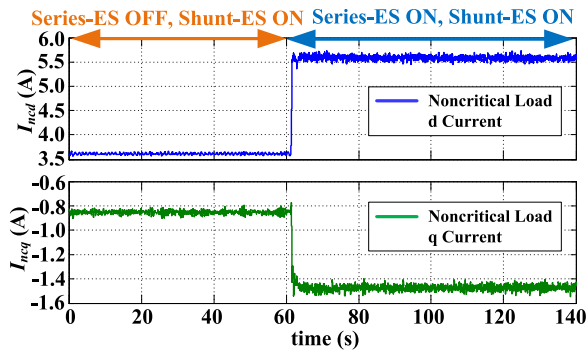


Fig. 17. Experimental active current ( $I_{ncd}$ ) and reactive current ( $I_{ncq}$ ) of the noncritical load in voltage suppression mode.

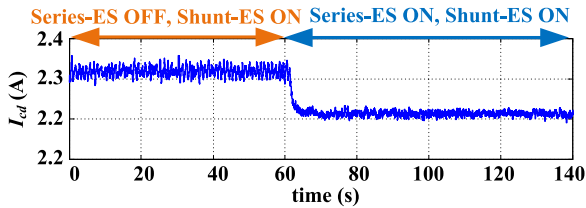


Fig. 18. Experimental active current of the critical load in voltage suppression mode.

noncritical load current and the series compensation voltage is restricted to  $90^\circ$  or  $270^\circ$ .

Other experimental results of the ES-B2B are included in Figs. 16–18. Fig. 16 shows that the Shunt-ES of the ES-B2B provides a small active current ( $I_{Shunt-ES,d}$ ) to cover the circuit power loss in the first 60 s (when the Series-ES is not activated yet). At  $t = 60$  s, the Series-ES is activated to suppress the

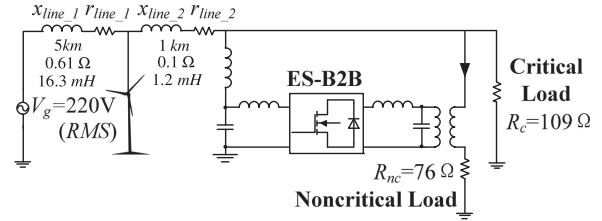


Fig. 19. Configuration of a weak grid.

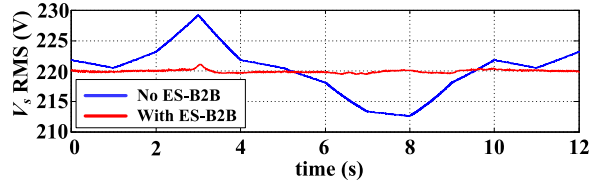


Fig. 20. Simulated mains voltage with and without ES-B2B.

mains voltage. As indicated by Fig. 14, the Series-ES generates a compensation voltage out of phase with the mains voltage. This compensation voltage increases the noncritical load voltage. The active and reactive current of the noncritical load ( $I_{ncd}$  and  $I_{ncq}$ ) in Fig. 17 shows that the power of the noncritical load is increased in order to reduce the mains voltage. Meanwhile, the Shunt-ES increases its active current (see Fig. 16). Since the mains voltage is restored from 115 to 110 V, the active current of the critical load is reduced after  $t = 60$  s as shown in Fig. 18.

### C. Operation of the ES-B2B in a Weak Grid (Simulation Study)

In this section, a simulation study has been conducted to examine the voltage regulation function of ES-B2B in a weak power grid with large penetration of intermittent renewable energy sources. The configuration and specifications are given in Fig. 19. The renewable energy source is modeled as a current source that generates fluctuating current into the grid. The ES-B2B is implemented to smooth the voltage fluctuation. The Series-ES is connected in series with a noncritical load via an isolation transformer. The Shunt-ES is attached to the mains via an inductor. A critical load of resistive type is connected to the mains. The circuit model of the weak grid and the ES-B2B is developed in MATLAB/SIMULINK. The model of ES-B2B has a higher voltage rating and thus can be implemented in a typical distribution system with a nominal mains voltage of 220 V (RMS). The dc voltage of ES-B2B is set at 660 V. The voltage of Series-ES is limited to 160 V (RMS).

The simulated mains voltage with and without ES-B2B are shown in Fig. 20. These results indicate that the ES-B2B can effectively mitigate the voltage fluctuation caused by the intermittent renewable power generation. The results in Fig. 21 show that the Series-ES of the ES-B2B actively changes the supply voltage of the noncritical load by generating an adjustable compensation voltage. The active current of the Shunt-ES shown in Fig. 22 indicates that the Shunt-ES can absorb or inject active power to keep a balanced power flow of ES-B2B and a stable dc-link voltage.

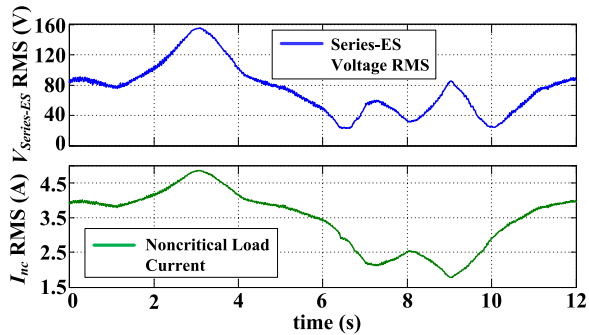


Fig. 21. Simulated voltage of Series-ES (upper trace) and the current of noncritical load (lower trace).

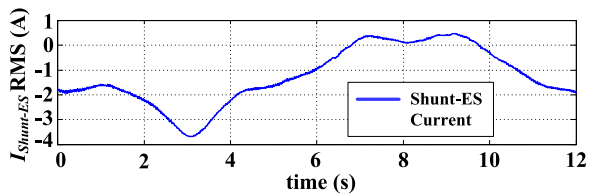


Fig. 22. Simulated current of the Shunt-ES.

## VII. CONCLUSION

This paper reports the first hardware implementation and control of an ES-B2B. Unlike the previous versions that is based on an inverter fed by a capacitor (ES-1) or a battery (ES-2), this version of ES is based on a back-to-back converter topology. This ES-B2B has the advantage over ES-1 by providing highly effective voltage support and suppression functions, while the ES-1 is less effective in voltage suppression. The proposed topology and control have been practically confirmed. The experimental results have verified the high performance of the ES-B2B for the regulation of the mains voltage. The simulation study of a weak power grid also indicates the usefulness of the ES-B2B in dynamically mitigating voltage fluctuation caused by intermittent renewable power generation.

## REFERENCES

- [1] P. P. Varaiya, F. F. Wu, and J. W. Bialek, "Smart Operation of smart grid: Risk-limiting dispatch," *Proc. IEEE*, vol. 99, no. 1, pp. 40–57, Jan. 2011.
- [2] I. Koutsopoulos and L. Tassiulas, "Challenges in demand load control for the smart grid," *IEEE Netw.*, vol. 25, no. 5, pp. 16–21, Oct. 2011.
- [3] A. Mohsenian-Rad, V. W. S. Wong, J. Jatskevich, R. Schober, and A. Leon-Garcia, "Autonomous demand-side management based on game-theoretic energy consumption scheduling for the future smart grid," *IEEE Trans. Smart Grid*, vol. 1, no. 3, pp. 320–331, Dec. 2010.
- [4] M. Parvania and M. Fotuhi-Firuzabad, "Demand response scheduling by stochastic SCUC," *IEEE Trans. Smart Grid*, vol. 1, no. 1, pp. 89–98, Jun. 2010.
- [5] M. Pedrasa, T. D. Spooner, and I. F. MacGill, "Scheduling of demand side resources using binary particle swarm optimization," *IEEE Trans. Power Systems*, vol. 24, no. 3, pp. 1173–1181, Aug. 2009.
- [6] F. Kienzle, P. Ahein, and G. Andersson, "Valuing investments in multi-energy conversion, storage, and demand-side management systems under uncertainty," *IEEE Trans. Sustain. Energy*, vol. 2, no. 2, pp. 194–202, Apr. 2011.
- [7] A. J. Conejo, J. M. Morales, and L. Baringo, "Real-time demand response model," *IEEE Trans. Smart Grid*, vol. 1, no. 3, pp. 236–242, Dec. 2010.

- [8] A. H. Mohsenian-Rad and A. Leon-Garcia, "Optimal residential load control with price prediction in real-time electricity pricing environments," *IEEE Trans. Smart Grid*, vol. 1, no. 2, pp. 120–133, Sep. 2010.
- [9] A. J. Roscoe and G. Ault, "Supporting high penetrations of renewable generation via implementation of real-time electricity pricing and demand response," *IET Renewable Power Gener.*, vol. 4, no. 4, pp. 369–382, Jun. 2010.
- [10] S. Y. R. Hui, C. K. Lee, and F. F. Wu, "Electric springs—A new smart grid technology," *IEEE Trans. Smart Grid*, vol. 3, no. 3, pp. 1552–1561, Sep. 2012.
- [11] C. K. Lee, B. Chaudhuri, and S. Y. Hui, "Hardware and control implementation of electric springs for stabilizing future smart grid with intermittent renewable energy sources," *IEEE J. Emerg. Sel. Topics Power Electron.*, vol. 1, no. 1, pp. 18–27, Mar. 2013.
- [12] Z. Akhtar, B. Chaudhuri, and S. Y. R. Hui, "Primary frequency control contribution through smart loads using reactive compensation," *IEEE Trans. Smart Grid*, vol. 6, no. 5, pp. 2356–2365, Sep. 2015.
- [13] Q. Wang, M. Cheng, Z. Zhen, and Z. Wang, "Steady-state analysis of electric springs with a novel  $\delta$  control," *IEEE Trans. Power Electron.*, vol. 30, no. 12, pp. 7159–7169, Dec. 2015.
- [14] C. K. Lee and S. Y. R. Hui, "Reduction of energy storage requirements for smart grid using electric springs," *IEEE Trans. Smart Grid*, vol. 4, no. 3, pp. 1282–1288, Sep. 2013.
- [15] S. Yan, S. C. Tan, C. K. Lee, B. Chaudhuri, and R. Y. Ron Hui, "Electric springs for reducing power imbalance in three-phase power systems," *IEEE Trans. Power Electron.*, vol. 30, no. 7, pp. 3601–3609, Aug. 2015.
- [16] K. R. Krishnanand, S. M. F. Hasani, J. Soni, and S. K. Panda, "Neutral current mitigation using controlled electric springs connected to microgrids within built environment," in *Proc. IEEE Energy Convers. Congr. Expo.*, 2014, pp. 2947–2951.
- [17] S. C. Tan, C. K. Lee, and S. Y. R. Hui, "General steady-state analysis and control principle of electric springs with active and reactive power compensations," *IEEE Trans. Power Electron.*, vol. 28, no. 8, pp. 3958–3969, Aug. 2013.
- [18] S. Yan, S. C. Tan, C. K. Lee, and S. Y. R. Hui, "Electric spring for power quality improvement," in *Proc. IEEE Appl. Power Electron. Conf. Expo.*, 2014, pp. 2140–2147.
- [19] Z. Akhtar, B. Chaudhuri, and S. Y. R. Hui, "Smart loads for voltage control in distribution networks," *IEEE Trans. Smart Grid*, early access.
- [20] K. T. Mok, S. C. Tan, and S. Y. R. Hui, "Decouple power angle and voltage control of electric springs," *IEEE Trans. Power Electron.*, vol. 31, no. 2, pp. 1216–1229, Feb. 2016.



**Shuo Yan** (S'13) received the B.Eng. degree from University of South China, Heng Yang, China, in 2007, and the M.Phil. degree from Southeast University, Nanjing, China, in 2010, both in electrical engineering. He is currently working toward the Ph.D. degree in electrical engineering in the Department of Electrical and Electronic Engineering, The University of Hong Kong, Hong Kong.

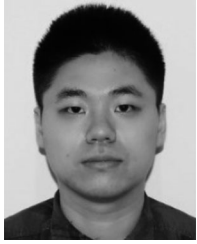
His current research interests include power electronic technology in smart grid, advance control of renewable energy sources, and microgrid.



**Chi-Kwan Lee** (M'08–SM'14) received the B.Eng. and Ph.D. degrees in electronic engineering from the City University of Hong Kong, Kowloon, Hong Kong, in 1999 and 2004, respectively.

He is currently an Assistant Professor in the Department of Electrical and Electronic Engineering, The University of Hong Kong, Hong Kong. Since 2010, He has been a Visiting Researcher with Imperial College London. He was a Postdoctoral Research Fellow in the Power and Energy Research Centre, National University of Ireland, Galway, Ireland, from 2004 to 2005. In 2006, he joined the Centre of Power Electronics, City University of Hong Kong, as a Research Fellow. In 2008–2011, he was a Lecturer of electrical engineering at the Hong Kong Polytechnic University. He is a co-inventor of the Electric Springs and planar electromagnetic interference filter. His current research interests include wireless power transfer, clean energy technologies, and smart grids.

Dr. Lee received the IEEE Power Electronics Transactions First Prize Paper Award for his publications on Mid-Range Wireless Power Transfer in 2015.



**Tianbo Yang** (S'15) received the B.Eng. and M.Phil. degrees in automation and control engineering from the Harbin Institute of Technology, Harbin, China, in 2012 and 2014, respectively. He is currently working toward the Ph.D. degree in the Department of Electrical and Electronic Engineering, The University of Hong Kong, Hong Kong.

His research interests include power electronic technologies in smart grid and energy storage system.



**Kwan-Tat Mok** (S'14) received the B.Eng. (Hons.) and M.Phil. degrees in electronic and information engineering from the Hong Kong Polytechnic University, Hong Kong, in 2009 and 2012, respectively. He is currently working toward the Ph.D. degree in the Power Electronics Research Group, Department of Electrical and Electronic Engineering, The University of Hong Kong, Hong Kong.

In 2007, he was an Engineering Trainee in Solomon Systech Limited, Hong Kong, for a one-year internship program. From September 2011 to

February 2013, he was an Embedded System Engineer in Cwlinux Limited, Hong Kong. From July to August 2015, he was a visiting postgraduate student in the Department of Electrical and Electronic Engineering, Imperial College London. His research interests include smart grid technologies, electric springs, and power converters for light-emitting diodes.



**Siew-Chong Tan** (M'06–SM'11) received the B.Eng. (Hons.) and M.Eng. degrees in electrical and computer engineering from the National University of Singapore, Singapore, in 2000 and 2002, respectively, and the Ph.D. degree in electronic and information engineering from the Hong Kong Polytechnic University, Hong Kong, in 2005.

From October 2005 to May 2012, he was a Research Associate, Postdoctoral Fellow, Lecturer, and Assistant Professor in the Department of Electronic and Information Engineering, Hong Kong Polytechnic

University, Hong Kong. From January to October 2011, he was a Senior Scientist in the Agency for Science, Technology and Research, Singapore. He is currently an Associate Professor in the Department of Electrical and Electronic Engineering, The University of Hong Kong, Hong Kong. He was a Visiting Scholar at Grainger Center for Electric Machinery and Electromechanics, University of Illinois at Urbana-Champaign, Champaign, from September to October 2009, and an Invited Academic Visitor of Huazhong University of Science and Technology, Wuhan, China, in December 2011. His research interests include power electronics and control, light-emitting diode lightings, smart grids, and clean energy technologies. He is a coauthor of the book entitled *Sliding Mode Control of Switching Power Converters: Techniques and Implementation* (Boca Raton, FL, USA: CRC Press, 2011).

Dr. Tan serves extensively as a reviewer for various IEEE/IET transactions and journals on power, electronics, circuits, and control engineering. He is an Associate Editor of the IEEE TRANSACTIONS ON POWER ELECTRONICS.



**Balarko Chaudhuri** (M'06–SM'11) received the Ph.D. degree in electrical and electronic engineering from Imperial College London, London, U.K., in 2005.

He is currently a Senior Lecturer at the Control and Power Research Group, Imperial College London. His research interests include power systems stability, grid integration of renewables, high-voltage direct current, flexible ac transmission system, demand response, and smart grids.

Dr. Chaudhuri is an Editor of the IEEE TRANSACTIONS ON SMART GRID and an Associate Editor of the IEEE SYSTEMS JOURNAL, and Elsevier's *Control Engineering Practice*. He is a Fellow of the Institution of Engineering and Technology and a member of the International Council on Large Electric Systems (CIGRE).



**S. Y. (Ron) Hui** (M'87–SM'94–F'03) received the B.Sc. (Eng.) (Hons.) degree from the University of Birmingham, Birmingham, U.K., in 1984, and the D.I.C. and Ph.D. degrees from Imperial College, London, U.K., in 1987.

He is currently the Philip Wong Wilson Wong Chair Professor at the University of Hong Kong, Hong Kong, and a part-time Chair Professor at Imperial College London. He has published more than 300 technical papers, including more than 220 refereed journal publications. Over 60 of his patents have

been adopted by industry.

Dr. Hui is an Associate Editor of the IEEE TRANSACTIONS ON POWER ELECTRONICS and IEEE TRANSACTIONS ON INDUSTRIAL ELECTRONICS, and an Editor of the IEEE JOURNAL OF EMERGING AND SELECTED TOPICS IN POWER ELECTRONICS. His inventions on wireless charging platform technology underpin key dimensions of Qi, the world's first wireless power standard, with freedom of positioning and localized charging features for wireless charging of consumer electronics. He received the IEEE Rudolf Chope R&D Award from the IEEE Industrial Electronics Society and the IET Achievement Medal (The Crompton Medal) in 2010, and IEEE William E. Newell Power Electronics Award in 2015. He is a Fellow of the Australian Academy of Technological Sciences & Engineering and also the Royal Academy of Engineering, U.K.